# INTERNATIONAL STANDARD

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# Plain bearings — Quality assurance of thin-walled half bearings — Selective assembly of bearings to achieve a narrow clearance range

Paliers lisses — Assurances qualité des demi-coussinets minces — Assemblage sélectif des paliers pour obtenir un jeu faible

Literature de la paliers pour obtenir un jeu faible

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This document was prepared by Technical Committee ISO/TC 123, *Plain bearings*, Subcommittee SC 5, *Quality analysis and assurance*.

This second edition cancels and replaces the first edition (ISO 13778:1999), which has been technically revised.

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# Plain bearings — Quality assurance of thin-walled half bearings — Selective assembly of bearings to achieve a narrow clearance range

# 1 Scope

This document specifies the selective assembly of bearings (in accordance with ISO 3548(1).

The bearing diametral clearance is determined by the housing diameter, journal diameter and the wall thickness of the two half bearings. Typically, these components will have a total tolerance "stack up" of  $50~\mu m$  to  $60~\mu m$ . Current engine development and in particular, the desire for improved engine refinement, has provided a need to decrease the clearance range due to the tolerance "stack up". This document suggests various schemes of selective assembly to achieve such ranges.

# 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 3548-1, Plain bearings — Thin-walled half bearings with or without flange — Part 1: Tolerances, design features and methods of test

ISO 4378-1, Plain bearings — Terms, definitions, classification and symbols — Part 1: Design, bearing materials and their properties

#### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 4378-1 and the following apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at <a href="http://www.electropedia.org/">http://www.electropedia.org/</a>
- ISO Online browsing platform: available at <a href="http://www.iso.org/obp">http://www.iso.org/obp</a>

#### 3.1

#### theoretical bearing diametral clearance

C

difference between the housing diameter,  $D_{\rm H}$ , less twice the half bearing wall thickness (3.3),  $s_3$ , and the journal diameter (3.4),  $D_{\rm I}$ 

$$C = D_{H} - (2s_{3} + D_{J})$$

#### 3.2

#### housing diameter

 $D_{\rm H}$ 

diameter of the housing with no bearing fitted measured perpendicular to the split line

#### 3.3

#### bearing wall thickness

wall thickness measured at 90° from the split line (at the "crown")

Note 1 to entry: If two measurements are made, the larger of the two is used.

#### 3.4

## journal diameter

diameter of the finished shaft measured at a position to give maximum diameter

#### 3.5

#### tolerance

range between the upper and lower limits specified on the drawing

#### 3.6

#### housing swell

expansion of a housing bore caused by the interference fit of the bearings

# Housing swell and thermal expansion

0115013118:2011 Housing swell is defined as the "expansion of a housing bore, caused by the interference fit of the bearings". When two half bearings are assembled into a housing and the housing is bolted up, the assembled bore will be slightly greater than the arithmetical subtraction of the two bearing wall thicknesses from the housing diameter as measured before the bearing is fitted. Housing swell is generally of the order of a few micrometres. Maximum housing swell will occur with a combination of maximum bearing overstand (nip) and minimum housing diameter. It is prudent to measure actual housing swell by carrying out fitting tests. Actual housing deformation may also be affected by the degree of control of bolt tension.

With light alloy housings, the housing swell may be larger, due not only to the lower modulus of elasticity but also to thermal expansion.

Allowance for housing swell and thermal expansion has to be made when setting the bearing diametral clearance.

# Measurement and identification

# 5.1 Housings and journals

Specific measurement of each housing and journal may be necessary in more complex grading schemes. While bearings will be graded according to only the crown wall thickness, journals in particular may have to be measured in several places, both axially and circumferentially, to ascertain the mean journal diameter. The crown housing diameter may be the only housing measurement necessary. With grade tolerances of a few micrometres, accurate measurement with minimal dirt and constant temperature is necessary.

Traditionally, crankshaft journals of different grades have been identified with a dab of paint or ink adjacent to the journal. Housings have been similarly identified. Such a method relies upon the visual discrimination of the operator and this may on occasions be unreliable. One alternative is to bar or dot code the housing and/or journal with either adhesive labels or by etching. Another is to store the data on computer for retrieval at assembly stage.

#### 5.2 Bearings

If bearing grades with wall thickness tolerances of less than the normal process capability are required, then consideration shall be given as to how the bearings are graded and identified. The part number is stamped upon the bearing prior to final wall thickness machining. Additional stamping after bearing grading is not feasible as this will create high spots of wall thickness. The usual practice is to mark the bearing side face after grading with a permanent colour code or with other suitable methods.

# 6 Suggested schemes for fitting

#### 6.1 General

The selective assembly of bearings shall be in accordance with ISO 3548-1.

Before choosing the scheme for selectively fitting bearings, it is first necessary to set the desired clearance range. As a general rule, the narrower the clearance range, the more complex the grading scheme will be and the tighter the tolerance on each component. As an example, if a clearance range of 24  $\mu m$  is required, this could entail grade tolerances of 6  $\mu m$ , while with a clearance range of 32  $\mu m$ , grade tolerances of 8  $\mu m$  would be acceptable.

While it may be desirable from the design viewpoint to achieve a very narrow clearance range, there may come a point at which perceived performance gains from working very close to the desired mean clearance become offset by the cost and complexity of the selective fitting scheme.

While such schemes are feasible for OE engine assembly, they are not practical for replacement bearings where the bearings are packed in sets of similar sizes.

Other points to consider are as follows.

- a) Due to the normal distribution of journal and housing sizes, the required quantity of each bearing grade will not necessarily be equal. Carefully controlled scheduling will be necessary in order to minimize bearing stocks and prevent shortages of particular bearing grades.
- b) Intermediate grades can be formed by fitting together half bearings from adjacent grades. This can significantly increase the flexibility of the system.
- c) If it is necessary to grade bearings by measurement after final wall thickness machining, then overlapping bearing grades are permissible and in fact allow the bearing supplier flexibility in achieving correct quantities of each bearing grade.
- d) When choosing a grading scheme, the difference in process capability for wall thickness between bimetallic and multi-layer should be taken into account.

The schemes described in 6.2 to 6.7 are examples only.

# 6.2 Scheme 1: Standard application, without grading

The clearance shall be determined by the limitations of normal process capability (see <u>Table 1</u>).

Housing diameter, *D*<sub>H</sub>: not graded

Journal diameter,  $D_{J}$ : not graded

Bearing wall thickness, s<sub>3</sub>: not graded

Table 1 — Standard application; without grading

Dimensions in millimetres

Grade	Without grading	
$D_{ m H}$	50,000 to 50,018	
$D_{J}$	46,000 to 46,018	
<i>s</i> <sub>3</sub>	1,972 to 1,978	
С	0,026 to 0,074	

### 6.3 Scheme 2: Grading of bearings

Scheme 2 is applicable where a slight reduction in the clearance tolerance is required. The bearings are graded to effectively reduce the tolerance of the grade (see <u>Table 2</u>).

Housing diameter,  $D_H$ : not graded

Journal diameter,  $D_{J}$ : not graded

Bearing wall thickness,  $s_3$ : three grades of 4  $\mu$ m

Table 2 — Grading of bearings

Dimensions in millimetres

	Grade	A	В	С
	$D_{H}^{a}$	50,000 6 50,018		
	$D_{J}^{\mathrm{a}}$	46,000 to 46,018		
	<i>s</i> <sub>3</sub>	1,970 to 1,974	1,974 to 1,978	1,978 to 1,982
	C <sup>b</sup>	0,026 to 0,070		
а	Without grading.	40;		
b	According to the	selection procedure.		

Depending on the selection procedure fit as a bearing pair, either two of grade B or one of grade A and one of grade C.

NOTE 1 The scheme is simple to administer.

NOTE 2 Compared to scheme 1, the clearance range of 0,026 mm to 0,074 mm is reduced to 0,026 mm to 0,070 mm.

# 6.4 Scheme 3: Grading of bearings and journals or housings

The housing or the journal is graded, usually into two or three grades and the bearings are graded into a similar number of grades (see <u>Table 3</u>).

Housing diameter,  $D_H$ : not graded

Journal diameter,  $D_1$ : three grades of 6  $\mu$ m grade tolerance

Bearing wall thickness, *s*<sub>3</sub>: three grades of 4 μm grade tolerance

Table 3 — Grading of bearings and journals or housings

Dimensions in millimetres

Grade	A	В	С
$D_{\mathrm{H}}^{\mathrm{a}}$	50,000 to 50,018		
$D_{J}$	46,000 to 46,006	46,006 to 46,012	46,012 to 46,018
<i>s</i> <sub>3</sub>	1,984 to 1,980	1,981 to 1,977	1,978 to 1,974
С	0,026 to 0,058		
a Without grading.			

NOTE 1 The spacing of each bearing grade is determined by the spacing of each journal grade in order to achieve an identical clearance range for each combination.

NOTE 2 Compared to scheme 2, the clearance range of 0,026 mm to 0,070 mm is reduced to 0,026 mm to 0,058 mm.

NOTE 3 Overlapping grades are used effectively.

NOTE 4 The scheme is simple to administer.

# 6.5 Scheme 4: Unmixed bearings (Matrix scheme)

Housing and journal diameter both graded with equal grade tolerances. With an equal number of housing and journal grades, the matrix is symmetrical and the distribution of bearings will be even. The bearing wall thickness grade tolerance is half that of the housing to journal diameter grade tolerance (see <u>Table 4</u> and <u>Table 5</u>).

Housing diameter,  $D_H$ : three grades of 6  $\mu$ m grade tolerance

Journal diameter,  $D_{\rm I}$ : three grades of  $\theta$  µm grade tolerance

Bearing wall thickness,  $s_3$ : five grades of 3 µm grade tolerance

**Table 4** — Unmixed bearings

Dimensions in millimetres

Grade	A CO	В	С	D	Е
$D_{\mathrm{H}}$	50,000 to <b>50,00</b> 6	50,006 to 50,012	50,012 to 50,018	_	_
$D_{J}$	46,000 to 46,006	46,006 to 46,012	46,012 to 46,018	_	_
<i>s</i> <sub>3</sub>	1,975 to 1,978	1,978 to 1,981	1,981 to 1,984	1,984 to 1,987	1,987 to 1,990
С	70,	0,026 to 0,044			

Table 5 — Bearing grades

	Bearing grade according to <u>Table 4</u>			
Journal grade	Housing grade			
	A	В	С	
A	C + C	D + D	E + E	
В	B + B	C + C	D + D	
С	A + A	B + B	C + C	

NOTE 1 Many bearing grades may be required, giving difficulty in discerning the colour shades involved.

NOTE 2 Compared to scheme 3, the clearance range 0.026~mm to 0.058~mm is reduced to 0.026~mm to 0.044~mm.