Power Presses: General Purpose, Single Action, Straight Side Type

AN AMERICAN NATIONAL STANDARD



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AN AMERICAN NATIONAL STANDARD



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CONTENTS

Fore	word	V
Com	mittee Roster	vi
Corr	respondence With the B5 Committee	vii
1	Scope, Purpose, and Application	20
		V
2	Definitions and Terminology	1
	٠ <u>٠</u> ٠	,
3	Metric/U.S. Customary Rationalization	1
4	Press Characteristics	1
5	Tooling Related Characteristics	3
6	Acceptance Conditions	13
	•	
7	Health and Safety	16
_		
8	Information and Instructions	16
•	Definitions and Terminology Metric/U.S. Customary Rationalization Press Characteristics Tooling Related Characteristics Acceptance Conditions Health and Safety Information and Instructions Declaration of Manufacturer's Compliance	10
9	Declaration of Manufacturer's Compliance	19
10	Defevence Standards	19
10	Reference Standards	19
Figu	Peclaration of Manufacturer's Compliance 1	
1	Slide Connections for Single-Point, Two-Point, and Four-Point Presses	2
2	Drives for Single-Point, Two-Point, and Four-Point Presses	3
3	Typical Construction of a Mechanical Press	4
4	Typical Construction of a Hydraulic Press	4
5	Typical Bolster	15
6	Typical Slide ().	15
7	Headed Pressure Pin	17
8	Headed Pressure Pinhole	17
9	Pressure Pinhole Location Identification System	18
10	Establishing the Bed as the Datum Plane	18
11	Bolster Flatness and Parallelism	19
12	Checking Parallelism From Slide Face to Bed or Bolster Surface	19
13	Checking Squareness of Slide Travel	20
14	Leveling the Slide Using Load Cells	20
15	Press Data Plate: Mechanical Press	21
16	Press Data Plate: Hydraulic Press	21
17	Counterbalance Data Plate	21
18	Die Cushion Data Plate	22
19	Press Designation System	22
20	Press Capability Graph (Metric)	23
21	Press Capability Graph (U.S. Customary)	24
Table		
1	Standard Capacity Ratings	1
2	Standard Rating Points	2

Press Speed/Drive Motor Relationship	2
Usable Flywheel Energy	3
Stroke and Die Space Dimensions: Mechanical Power Press	5
	5
	6
	7
	7
	8
	9
	9
	10
	11
	12
	12
Deleter Handling Floies: Two-rollit and Four-rollit Fless	13
Dolster Handling Hook Dimensions	
	14
Number of 1-Slots	16
Plain Pressure Pin.	16
Pressure Pinhole Patterns	17
Pressure Pinhole Plug	18
Mechanical Power Press Capacity Above Rating Point of (2.7 mm (0.5 in.)	25
	26
	27
Usable Flywheel Energy	28
Bed and Slide Deflection	29
Offset Loading of a Mechanical Press Slide	30
ile and the second of the seco	
nandatory Annendices	
Metric/U.S. Customary Conversion	31
Comparison of Capacity Ratings Between Historical IIC and ISO	
Standards	32
- Charles and the control of the con	02
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Comparison of Capacity Ratings Between Historical JIC and ISO Standards	
1	Stroke and Die Space Dimensions: Mechanical Power Press. Bed and Slide Dimensions: Single-Point Press Bed and Slide Dimensions: Two-Point and Four-Point Press Bolster Locating Pin Dimensions Spacing of Bolster Locating Pinholes: Single-Point Press Spacing of Bolster Locating Pinholes: Two-Point and Four-Point Press Bolster Mounting Slot Dimensions Spacing of Bolster Mounting Slots: Single-Point Press Spacing of Bolster Mounting Slots: Two-Point and Four-Point Press Bolster Mounting Bolt Dimensions. Bolster Handling Holes: Single-Point Press Bolster Handling Holes: Two-Point and Four-Point Press Bolster Handling Hook Dimensions Bolster Handling Hook Bolt Dimensions Number of T-Slots Plain Pressure Pin Pressure Pinhole Patterns Pressure Pinhole Patterns Pressure Pinhole Plug datory Appendices Mechanical Power Press Capacity Above Rating Point of 12.7 mm (0.5 in.) Mechanical Power Press Capacity Above Rating Point of 1.6 mm (0.06 in.) Usable Flywheel Energy Bed and Slide Deflection Offset Loading of a Mechanical Press Slide Metric/U.S. Customary Conversion

FOREWORD

Recognizing the need for a standard for mechanical power presses, the ASME Committee on Machine Tools and Components (B5) established in December 1973, Technical Committee 30 to develop an American National Standard addressing the interchangeability of bolsters, press tooling, and mounting provisions between general purpose presses of comparable bed size, capacity, and type.

The B5-TC30 membership consists of a balance between manufacturers, users, accessory suppliers and others associated with power presses. The technical committee's work was based on the Joint Industry Conference (JIC) Press Room Standards, once the most widely used document, to develop a standard for mechanical power presses, and basic data submitted by U.S. manufacturers of power presses.

In April 1983, the committee completed the final draft of "Standard for Straight Side Type Presses (Metric)." This draft was not submitted for approval before the committee became inactive.

In 1995, Technical Committee 30 was reestablished to continue the pursuit of the original objectives set forth in 1973. The scope of the Standard was expanded to include hydraulic power presses.

ASME B5.61-2003 was approved by the American National Standards Institute on July 7, 2003.

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(The following is the roster of the Committee at the time of approval of this Standard.) KB5.612003

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General. ASME Standards are developed and maintained with the intent to represent the consensus of concerned interests. As such, users of this Standard may interact with the Committee by proposing revisions, and attending Committee meetings. Correspondence should be addressed to:

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Proposing Revisions. Revisions are made periodically to the Standard to incorporate changes that appear necessary or desirable, as demonstrated by the experience gained from the application of the Standard. Approved revisions will be published periodically.

The Committee welcomes proposals for revisions to this Standard. Such proposals should be as specific as possible, citing the paragraph number(s), the proposed wording, and a detailed description of the reasons for the proposal, including any pertinent documentation.

Attending Committee Meetings. The B5 Main Committee regularly holds meetings, which are open to the public. Persons wishing to attend any meeting should contact the Secretary of the B5 Main Committee.

vii

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POWER PRESSES: GENERAL PURPOSE, SINGLE ACTION, STRAIGHT SIDE TYPE

1 SCOPE, PURPOSE, AND APPLICATION

1.1 Scope

This Standard applies to hydraulic and mechanical power presses commonly referred to by the metal-working industry as *General Purpose*, *Single Action*, *Straight Side Type Power Presses* that, by means of dies or tooling attached to the slide and bolster, are used to shear, punch, form, or assemble metal or other materials.

The following types of presses are excluded from this Standard:

- (a) air (pneumatic)
- (b) bench
- (c) eyelet machines
- (d) forging
- (e) four slide machines
- (f) gap frame
- (g) knuckle joint
- (h) multiple action
- (i) multiple slide
- (j) spotting
- (k) transfer feed
- (l) turret punching

1.2 Purpose

The purpose of this Standard is to define and describe power presses and their interface, and to permit interchangeability of bolsters, dies, and tooling components between presses of comparable type, size, and capacity.

1.3 Application

Any power press described herein and referred to as an American National Standard Power Press shall comply with the applicable requirements delineated in this Standard.

2 DEFINITIONS AND TERMINOLOGY

Terms used in this Standard are defined in ASME B5.49, Glossary of Power Press Terms.

3 METRIC/U.S. CUSTOMARY RATIONALIZATION

3.1 Metrication

All units of dimension and capacity stated herein are in accordance with ASME B5.51M, Preferred SI Units

Table 1 Standard Capacity Ratings

Single-Poi	nt Press	Two-Point	Four-Poin	Four-Point Press	
kN tons		kN tons		kN	tons
250	30		გე.		
500	55	500	55		
1 000	110	1 000	110		
1 600	180	1 600	180		
2 000	225	2 000	225		
2 500	280	2 500	280	2 500	280
4 000	450	4 000	450	4 000	450
6 300	710	6 300	710	6 300	710
10 000	1,125	10 000	1,125	10 000	1,125
	X	16 000	1,800	16 000	1,800
1,5		20 000	2,250	20 000	2,250
	• • •	25 000	2,810	25 000	2,810

for Machine Tools. Approximate U.S. Customary units are historical standards and are for reference only. Wherever used in this Standard, the unit *tons* denotes U.S. tons

3.2 Metric/U.S. Customary Conversion

Nonmandatory Appendix A provides conversion multipliers applicable to this Standard.

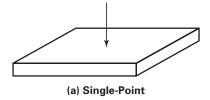
4 PRESS CHARACTERISTICS

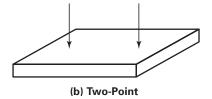
4.1 Rated Capacity

Standard capacity ratings shall be as specified in Table 1 (see also Fig. 1). See Nonmandatory Appendix B for historical comparison of capacity ratings.

4.2 Rating Points (Mechanical Power Press)

- (a) Standard rating points shall be as specified in Table 2.
- (b) Drive design shall be based on providing the torque, which produces the rated press capacity at the rating point (see Fig. 2).
- (c) Press capacity at points other than the rating point are shown in
- (1) Mandatory Appendix I for presses rated at 12.7 mm ($\frac{1}{2}$ in.)
- (2) Mandatory Appendix II for presses rated at 6.3 mm ($\frac{1}{4}$ in.)





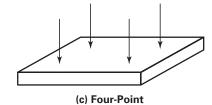


Fig. 1 Slide Connections for Single-Point, Two-Point, and Four-Point Presses

Table 2 Standard Rating Points

	Rating Point			
Press Type	mm	in.		
Flywheel drive	1.6	1/16		
Single end drive Twin end drive blanking press Eccentric gear blanking press	6.3	1/4		
Twin end drive Eccentric gear	12.7	1/2		

(3) Mandatory Appendix III for presses rated at 1.6 mm ($\frac{1}{16}$ in.)

4.3 Energy Capacity (Mechanical Power Press)

- **4.3.1 Function of the Flywheel.** The energy required for performing press operations is stored in the flywheel. During the working portion of the press cycle, the flywheel slows down as it supplies the required energy to the drive train.
- **4.3.2 Function of the Drive Motor.** The drive motor restores flywheel energy during the norworking portion of the press cycle, which may include the interval between press cycles for presses operating in single stroke modes.
- **4.3.3 Drive Motor Selection.** The selection of the drive motor is dependent upon the energy requirements. Factors determining the energy requirements are:
 - (a) rated capacity
 - (b) press speed (strokes per minute)
 - (c) press stroke

Based on the optimum slide velocity for the material being worked, a longer stroke press will be required to operate at a slower speed than a shorter stroke press. The longer the stroke, the deeper the draw that can be made, and the greater the energy required to sustain the press through the depth of the draw. Table 3 specifies typical press speed/drive motor relationships.

4.3.4 Drive Motor/Flywheel Relationship. The usable energy that a flywheel can supply is a function of the ability of the drive motor to tolerate slowdown without overheating. The usable flywheel energy, expressed as

Table 3 Press Speed/Drive Motor Relationship

Press Speed, spm	Type of Motor Required
10 spm or less Between 10 spm and 30 spm 30 spm or more	Design D, 8% – 13% slip Design D, 5% – 8% slip Design B, 3% – 5% slip

a percentage of total flywheel energy, is a function of the motor slowdown. Table 4 specifies the properties of the three types of single speed drive motors that are most commonly used on mechanical power presses. Mandatory Appendix IV provides a method for calculating the usable flywheel energy.

4.3.5 Variable Speed Presses. Unless otherwise specified by the purchaser, usable flywheel energy for variable speed presses shall be rated at one-half the maximum speed.

IMPORTANT: The energy range for a variable speed press varies as the square of the speed range. For example, a speed range of 3:1 would provide an energy range of 9:1. For a press with a speed range of 20 spm to 60 spm, the following would be the energies available:

SPM	Energy Available, %
20	45
30	100
60	400

4.4 Structural Capacity

(a) Bed and slide design shall be based on symmetrically distributed loading of the bed and slide over two-thirds of the left-to-right and front-to-back area dimensions of the bed and the slide, respectively. The bed size is normally the bolster area.

NOTE: Tool design should be based on distributing full capacity loading of the press over at least two-thirds of the die space. Dies that do not span the slide connections will result in overload of the bed and slide members at full press capacity.

- (*b*) Bed and slide design shall be based on the following allowable deflection criteria:
- (1) for other than progressive die presses, deflection of the bed and slide to be within 0.17 mm/m (0.002 in./ft) of the left-to-right dimension
 - (2) for progressive die presses

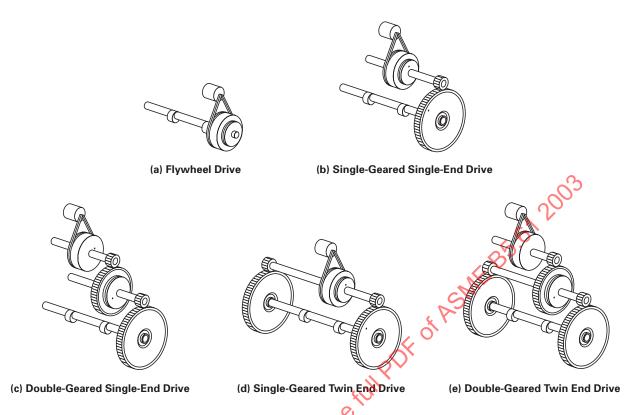


Fig. 2 Drives for Single-Point, Two-Point, and Four-Point Presses

Table 4 Usable Flywheel Energy

Motor Design	Motor Slip, %	Maximum Flywheel Slowdown, %	Usable Flywheel Energy, %
В	3 to 5	10	19
D	5 to 8	15	28
D	8 to 13	20	36

- (a) deflection of the bed and slide to be within 0.08 mm/m (0.001 in 7ft) of the left-to-right dimension, for dimensions up to 3 000 mm (118 in.)
- (b) deflection of the bed and slide to be within 0.12 mm/m (0.0015 in./ft) of the left-to-right dimension, for dimensions greater than 3 000 mm (118 in.)
- (3) measurement of deflection with a distributed load cannot be duplicated by testing. Mandatory Appendix V suggests an empirical method of simulating bed and slide loading for testing purposes. This measurement is only done upon the request and agreement of the purchaser.

4.5 Loading of a Press Slide

4.5.1 Mechanical Press. For multiple-point presses, the press slide and its connections shall be designed to withstand offset loading as follows (see Mandatory Appendix VI):

- (a) for a two-point mechanical press, 60% of the rated capacity under each connection
- (b) for a four-point mechanical press, 35% of the rated capacity under each connection
- (c) the total load on the slide shall not exceed the total rated press capacity

EXAMPLE: For a 4 000 kN press two-point press:

- (1) 4 000 kN \times 0.6 = 2 400 kN maximum force can be applied by one connection
- (2) $4\,000~kN-2\,400~kN=1\,600~kN$ maximum force can be applied by the other connection

Mechanical presses shall be provided with hydraulic overloads rated at 110% of press capacity.

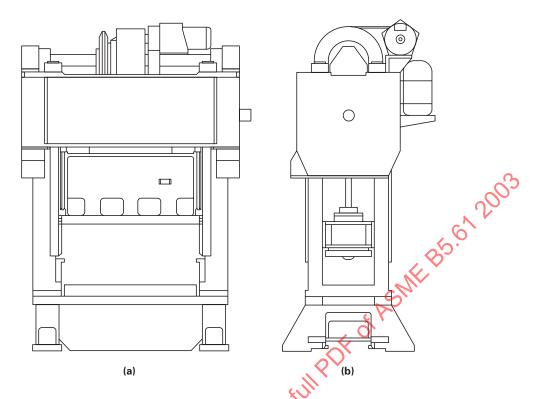
4.5.2 Hydraulic Press. Nominal press force (kN) multiplied by 0.075 m equals maximum off-center load (kN·m). Nominal press force (tons) multiplied by 3 in. equals maximum off-center load (in.-tons). Calculation of an off-center force requires consideration.

EXAMPLE: To determine the load that can be applied at 0.5 m off-center for a $4\,000\ \text{kN}$ press:

- (1) $4\,000 \text{ kN} \times 0.075 \text{ m} = 300 \text{ kN} \cdot \text{m}$
- (2) $300 \text{ kN} \cdot \text{m} / 0.5 \text{ m} = 600 \text{ kN}$

5 TOOLING RELATED CHARACTERISTICS

See Figs. 3 and 4.



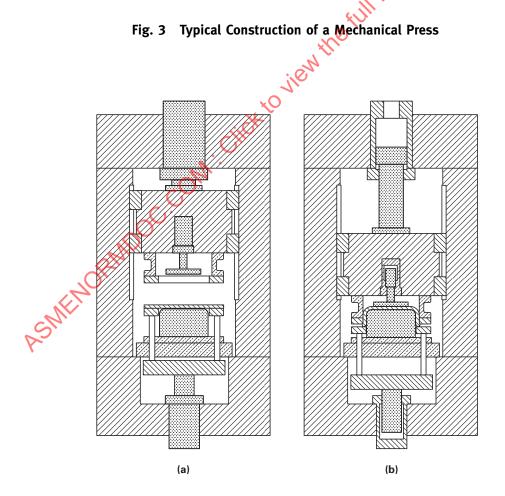


Fig. 4 Typical Construction of a Hydraulic Press

Nominal Bolster Thickness Slide Standard Maximum **Press** Stroke Stroke [Note (1)] Shutheight Adjustment Rated Capacity kΝ tons in. in. in. in. in. mm mm mm mm mm 1 000 1 600 2 000 2 500 4 000 6 300 250-300 (2) 10 - 1210 000 1,125 275-300 (3) 11-12 **N**36 16 000 1,800 1 000 20 000 2,250 1 000 1 200 25 000 2,810

Table 5 Stroke and Die Space Dimensions: Mechanical Power Press

NOTES:

- (1) Bolster thickness is based on steel.
- (2) 300 mm for 2 400 mm front-to-back or larger.
- (3) 300 mm for 2 200 mm front-to-back or larger.

Front-to-Back Front-to-Back Rated Capacity Left to Right Bed Slide kΝ tons mm in. mm in. in. mm 1 000 1 000 1 600 2 000 1 1 2 0 1 000 2 500 1 250 4 000 1 400 1 250 6 300 10 000 1,125 1 600 1 800 1 600

Table 6 Bed and Slide Dimensions: Single-Point Press

5.1 Stroke and Die Space Dimensions

Standard stroke lengths, die space heights, and slide adjustments shall be as specified in Table 5. (For hydraulic presses, no standards apply to stroke length or slide adjustment.)

5.2 Bed and Slide Dimensions

- (a) For presses with the slide driven by a single mechanical connection, or a single hydraulic piston, bed and slide dimensions shall be as specified in Table 6.
- (b) For presses with the slide driven by multiple mechanical connections, or multiple hydraulic pistons, bed and slide dimensions shall be as specified in Table 7.

5.3 Bed Openings

(a) For all presses, the left-to-right bed opening is 300 mm less than the left-to-right bed size.

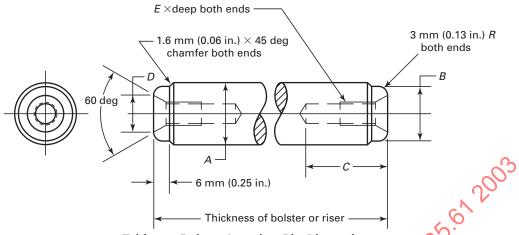
- (b) For presses from 250 kN up to 4 000 kN, the front-to-back bed opening is 300 mm less than the front-to-back bed size.
- (c) For presses from 4 000 kN up to 10 000 kN, the front-to-back bed opening is 450 mm less than the front-to-back bed size.
- (d) For presses from 10 000 kN through 25 000 kN, the front-to-back bed opening is 600 mm less than the front-to-back bed size.

5.4 Bolster Locating Pins

- (a) Material for locating pins shall be SAE 1020 cold rolled steel, carburized, and hardened.
- (b) Locating pin diameter tolerances shall be +0 −0.13 mm (−0.005 in).
- (c) Surface finish on locating pins shall be $R_a=3.2~\mu m$ (125 $\mu in.$) on diameters and $R_a=6.3~\mu m$ (250 $\mu in.$) on the ends.

Table 7 Bed and Slide Dimensions: Two-Point and Four-Point Press

								Fron	it to Back	(
Rated Capacity		Left to	Right			Two-Poir	nt Press	1			Four-Po	oint Press	
kN	tons	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.
250	30	800	32	600	24								
500	55	1 250	50	800	32								
1 000	110	1 250	50	800	32	900	36						
		1 600	60	900	36	1 000	40	1 120	42				
1 600	180	1 250	50	800	32	900	36					O _o)
1 000	100	1 600	60	900	36	1 000	40	1 120	42			000	
2 000	225	1 400	54	900	36	1 000	40						
2 000		1 600	60	900	36	1 000	40	1 120	42			O .	
		1 800	72	1 000	40	1 120	42	1 250	50		ొన్న	•	
2 500	280	1 600	60	1 000	40	1 120	42	1 250	50		Z, V		
		1 800	72	1 000	40	1 120	42	1 250	50				
		2 200	84	1 250	50	1 400	54			1 600	62		
		2 500	96	1 400	54					1 600	62		
		2 800	108							1 600	62	1 800	72
		3 100	120							1 800	72	2 000	78
4000	450	1 800	72	1 120	42	1 250	50		$-\mathcal{O}_{\ell}$				
		2 200	84	1 250	50	1 400	54		QY	1 600	62		
		2 500	96	1 400	54			(1 600	62	1 800	72
		2 800	108					<i>U</i> }		1 600	62	1 800	72
		3 100	120		• • •	• • •			• • •	1 800	72	2 000	78
6 300	710	2 200	84	1 250	50	1 400	54	11.		1 600	62		
		2 500	96	1 400	54		2			1 600	62	1 800	72
		2 800	108							1 600	62	1 800	72
		3 100	120				7.	• • •		1 800	72	2 000	78
		3 400	132	• • •		xO		• • •	• • •	2 000	78	2 200	84
		3 700	144	• • •		· 4	• • •	• • •	• • •	2 00	84	2 400	96
10 000	1,125	2 800	108		٠	-110		• • •		1 800	72	2 200	84
		3 100	120	• • •)	• • •	• • •		1 800	72	2 200	84
		3 400	132	• • •	~V	• • •	• • •	• • •	• • •	2 200	84	2 400	96
		3 700	144	٠ ر	1/2.	• • •	• • •	• • •	• • •	2 200	84	2 400	96 06
		4 000 4 600	156 180		<i>)</i>	• • •		• • •	• • •	2 200 2 400	84 96	2 400 2 600	96 102
		5 200	204	C_1						2 800	108	3 000	120
16 000	1 000		120										
16 000	1,800	3 100 3 400	132		• • •	• • •		• • •	• • •	2 200 2 200	84 84	2 400	 96
		3 700	144	• • •		• • •	• • •	• • •	• • •	2 200	84	2 400	96
		4 000	156					•••		2 400	96	2 600	102
		4 600	180							2 400	96	2 600	102
		5 200	204							2 800	108	3 000	120
20 000	2,250	3 400	132							2 200	84	2 400	96
_0 000	2,250	3 700	144							2 200	84	2 400	96
	P	4 000	156							2 400	96	2 600	102
	•	4 600	180							2 400	96	2 600	102
		5 200	204							2 800	108	3 000	120
25 000	2,810	3 700	144							2 200	84	2 400	96
		4 000	156							2 400	96	2 600	102
		4 600	180							2 400	96	2 600	102
		5 200	204							2 800	108	3 000	120



		Ra	ited Capacity	
	Through 1 00	00 kN (110 T)	C0ver 1 00	0 kN (110 T)
Dimension	mm	in.	mm	in.
Α	29	1.13	4	1.63
В	25	1.0	38	1.5
С	32	1.25	44.5	1.75
D	19	0.75	25	1.0
Ε	$M12 \times 25$ mm deep	$\frac{1}{2}$ -13 × 1 in. deep	M20 × 38 mm deep	$\frac{3}{4}$ -10 × 1.5 in. deep

- (d) Locating pinhole specifications shall be as follows?
- (1) for press capacities through 1 000 kN (110 tons): 30 mm (1.16 in.) diameter
- (2) for press capacities over 1 000 kN (110 tons): 43 mm (1.63 in.) diameter
- (e) Two holes shall be drilled through, with chamfer at top of 6 mm (0.25 in.) × 45 deg.
- (f) Locating pin dimensions shall be as specified in Table 8.
- (g) Spacing of locating pinholes for both bed and bolster shall be as specified in Tables 9 and 10.

5.5 Bolster Mounting Slots

- (a) Bolster mounting slot dimensions shall be as specified in Table 11.
- (b) Spacing of bolster mounting slots shall be as specified in Tables 12 and 13.

5.6 Bolster Mounting Bolts

- (a) Bolster mounting bolt specifications shall be as follows:
 - (1) length, *L*, and finish to be specified by purchaser
- (2) medium carbon alloy steel, hardened and tempered
- (3) tensile strength 1 000 MPa (150,000 psi) minimum, Brinell hardness 264–353
- (b) Bolster mounting bolt dimensions shall be as specified in Table 14.

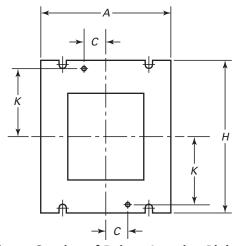


Table 9 Spacing of Bolster Locating Pinholes: Single-Point Press

	Left to	Right			Front to	o Back	
A			c	н			K
mm	in.	mm	in.	mm	in.	mm	in.
630	24	105	4.1	800	32	340	13.4
800	32	105	4.1	1 000	40	440	17.3
1 000	40	230	9	1 120	42	500	19.7
1 250	50	380	15	1 400	54	640	25.2
1 600	60	380	15	1 800	72	840	33

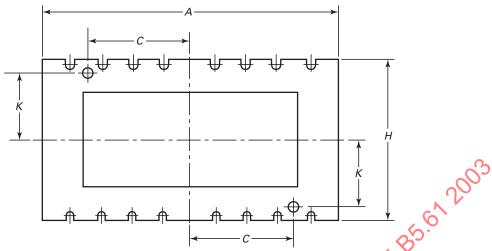


Table 10 Spacing of Bolster Locating Pinholes: Two-Point and Four-Point Press

	Left to	Right		Suggested Front to Back						
	A		•	Dimension, C		, h	H		К	
mm	in.	mm	in.	mm	in.	mm	in.	mm	in.	
800	32	230	9	300	11.8	600	24	240	9.4	
1 250	48	230	9	300	11.8	800	32	340	13.4	
1 400	54	230	9	300	11.8	900	36	390	15.3	
1 600	60	380	15	450	17.70	1 000	40	440	17.3	
1 800	72	535	21	600	23.6	1 120	42	500	19.7	
2 200	84	685	27	750	29.5	1 250	50	565	22.2	
2 500	96	840	33.1	900	35.4	1 400	56	640	25.2	
2 800	108	990	39	900 🜙	35.4	1 600	60	740	29.1	
3 100	120	1 145	45	1 050	41.3	1 800	72	840	33.1	
3 400	132	1 295	51	1 350	53.1	2 000	78	940	37	
3 700	144	1 450	57	1 500	59	2 200	84	1 040	40.9	
4 000	156	1 600	63	1 500	59	2 400	96	1 140	44.1	
4 600	180	1 900	74.8	1 800	70.9	2 600	102	1 240	48.8	
5 200	204	2 210	87	2 250	88.6	2 800	108	1 340	52.8	
			$O_{M_{\star}}$			3 000	120	1 440	56.7	

5.7 Bolster Handling Holes

Bolster handling holes shall be located as specified in Tables 15 and 16.

5.8 Bolster Handling Hooks

- (a) Bolster handling hooks shall meet the following requirements:
- (1) closed die drop forging: SAE fine grain, heat treated to Brinell hardness 186–241
- (2) inspected by ultrasonic and fluorescent magnetic particle method
 - (3) free from laps, seams, or other surface defects
- (4) no permanent set at a proof load of three times the lifting capacity, when loaded vertically
- (b) Bolster handling hook dimensions shall be as specified in Table 17.
- (c) Bolster handling hook bolts shall meet the following requirements:

- (1) medium carbon alloy steel, hardened and tempered
- (2) tensile strength 1 000 MPa (150,000 psi) minimum, Brinell hardness 302–352
- (*d*) Bolster handling hook bolt dimensions shall be as specified in Table 18.

5.9 Die Attachment

- (a) T-slots, bolts, and nuts shall conform to the requirements of ASME B5.1M, T-Slots Their Bolts, Nuts, and Tongues. The recommended T-bolt sizes are 20 mm (0.78 in.) for presses up to 1 000 kN (110 ton) and 24 mm (1 in.) for presses above 1 000 kN (110 tons).
- (*b*) T-slots shall be located on 150 mm (6 in.) centers. The middle T-slots are 75 mm (3 in.) to the right and to the left of the front-to-back centerline of the bolster and the slide. See Figs. 5 and 6 for a typical bolster and slide. Number of T-slots are specified in Table 19.

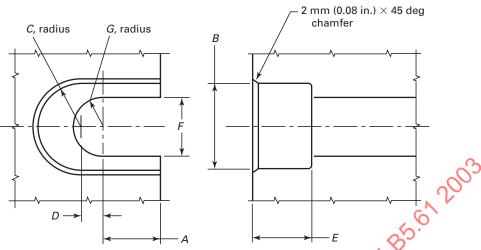


Table 11 Bolster Mounting Slot Dimensions

В	olt Size		ted acity		Α		В		С)	ري کې	E		F		G
SI	Customary	kN	tons	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.
M20	³ / ₄ – 10	250	30	24	0.94	34	1.34	17	0.67	10	0.39	20	0.79	24	0.94	12	0.47
M24	1 – 8	500	55	28	1.10	40	1.57	20	0.79	12	0.47	25	0.98	28	1.1	14	0.56
M30	$1^{1}/_{4} - 6$	>500	>55	34	1.34	50	1.97	25	0.98	15	0.59	30	1.18	34	1.34	17	0.68

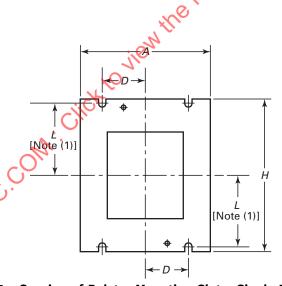


Table 12 Spacing of Bolster Mounting Slots: Single-Point Press

	Left to		Front to	Back.		
Α			D	H		
mm	in.	mm	in.	mm	in.	
630	24	150	5.9	800	32	
800	32	350	13.8	1 000	40	
1 000	40	450	17.7	1 120	42	
1 250	50	450	17.7	1 400	54	
1 600	60	600	23.6	1 800	72	

GENERAL NOTE: Mounting slots are symmetrical about the centerlines.

NOTE

(1) Calculate L based on dimension A in Table 11.

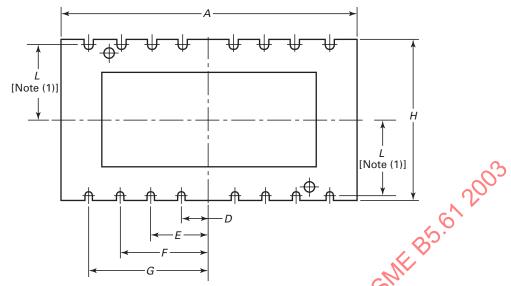


Table 13 Spacing of Bolster Mounting Slots: Two-Point and Four-Point Press

	4		D	E		F	-	6 €	i	ŀ	1
mm	in.	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.
800	32	350	13.8				0	>		600	24
1 250	50	450	17.7							800	32
1 400	54	600	23.6				80),			900	36
1 600	60	600	23.6				2,			1 000	40
1 800	72	300	11.8	750	29.5	<i>7</i> / <i>x</i>				1 120	42
2 200	84	300	11.8	900	35.4	N C				1 250	50
2 500	96	300	11.8	1 050	41.3	.01				1 400	54
2 800	108	300	11.8	1 050	41.3	110				1 600	60
3 100	120	300	11.8	900	35.4	1 200	47.2			1 800	72
3 400	132	300	11.8	900	35.4	1 500	59			2 000	78
3 700	144	300	11.8	900	35.4	1 650	65			2 200	84
4 000	156	300	11.8	900 🌈	35.4	1 650	65			2 400	96
4 600	180	300	11.8	900.	35.4	1 500	59	2 100	82.7	2 600	102
5 200	204	300	11.8	900	35.4	1 500	59	2 100	82.7	2 800	108
				Oli,						3 000	120

GENERAL NOTE: Mounting slots are symmetrical about the centerlines. NOTE:

(1) Calculate L based on dimension A in Table 11.

NOTE: For presses that conform to the historical JIC standards, the middle T-slot is on the front-to-back centerline of the bolster and the slide.

5.10 Pneumatic Die Cushions

Pneumatic die cushions, when provided, shall meet the following requirements:

- (a) Die cushion capacity shall be approximately 15% of the rated capacity of the press.
- (*b*) Pneumatic die cushion capacities shall be rated at 700 kPa (100 psi) of air pressure.
- (c) Die cushion stroke shall be approximately one third of the press stroke.
- (*d*) The distance between the die cushion pin plate and the top of the bed shall be 12.7 mm (0.50 in.) with tolerances of +0 -0.75 mm (-0.030 in.). Means shall be

provided, integral with the die cushion, to positively stop the die cushion stroke at its upper limit. With multiple die cushions within the press bed, measured total variation between die cushion pin plates at the upper limit of stroke shall not exceed 0.25 mm (0.010 in.).

- (e) Die cushion pin plate(s) shall be provided with a minimum wear surface Brinell hardness of 300.
- (f) Pneumatic die cushion pressure variation shall not exceed 20% during a complete press cycle.

5.11 Hydraulic Die Cushions

(a) Due to the wide variety of applications for hydraulic die cushions, no standards have been developed. Features that have been incorporated include the following:

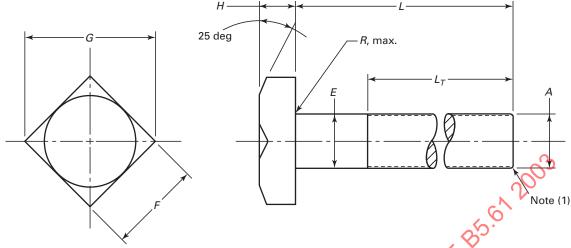


Table 14 Bolster Mounting Bolt Dimensions

				Bolt	Size		
		M20 (³ /	/ ₄ – 10)	M24.((1 – 8)	M30 $(1^{1}/_{4} - 7)$	
Di	mension/Description	mm	in.	mm	in.	mm	in.
Ε	Nominal diameter	20	0.75	24	1.0	30	1.25
F	Nominal head width	30	1.2	36	1.42	46	1.81
	Maximum head thickness	30	1.2	36	1.42	46	1.81
	Maximum head width	29	1.14	34.8	1.37	44.5	1.75
G	Minimum width across corners	39.8	1.57	47.8	1.88	61.1	2.4
Н	Nominal head thickness	14	0.55	16	0.63	20	0.79
	Maximum head thickness	14.5	0.57	16.7	0.66	20.8	0.82
	Minimum head thickness	13.4	0.53	15.3	0.6	19.2	0.76
R	Maximum radius	2	0.08	2	0.08	2	0.08
Α	Thread data:						
	Pitch	2.5	0.10	3	0.125	3.5	0.143
	Basic major diameter	19.6	0.75	23.95	1.0	29.95	1.25
	Basic pitch diameter	18.38	0.69	22.05	0.92	27.73	1.16
L_T	Minimum full thread length	50	2.0	58	2.3	70	2.8

NOTE:

- (1) 45 deg chamfer round point or first thread rolled undersize to facilitate assembly.
 - (1) programmable force throughout the stroke
- (2) programmable ejection function (hold-down feature)
 - (3) pre-acceleration to reduce slide impact
- (b) Die cushion capacity shall be a minimum of 15% of the rated capacity of the press.
- (c) Die cushion stroke shall be a minimum of onethird of the press stroke.
- (d) The distance between the die cushion pin plate and the top of the bed shall be 12.7 mm (0.50 in.) with tolerances of +0 -0.75 mm (-0.030 in.). Means shall be provided, integral with the die cushion, to positively stop the die cushion stroke at its upper limit. With multiple die cushions within the press bed, measured total variation between die cushion pin plates at the upper limit of stroke shall not exceed 0.25 mm (0.010 in.).

(e) Die cushion pin plate(s) shall be provided with a minimum wear surface Brinell hardness of 300.

5.12 Pressure Pins

- (a) Pressure pins shall meet the following requirements:
- (1) For normal service, material shall be SAE 1020 cold drawn steel.
- (2) For heavy service, the material shall be SAE 1020 cold drawn steel, carburized 1.3 mm (0.05 in.) to 1.5 mm (0.06 in.) deep and hardened to 50–60 Rockwell C Scale.
- (3) Tolerance of the diameter shall be +0 -0.13 mm (-0.005 in.).
 - (4) Ends shall be smooth, flat, and square to the pin.

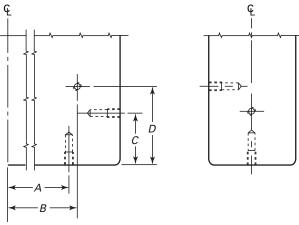


Table 15 Bolster Handling Holes: Single-Point Press

			 ←A · ←B Table 15	Bolste	er Hand	↓ ↓ ling Hol	les: Sing	gle-Point	Press	Q.	ري. دري.	2003	
Be Left to	•		ap Size Class 3	Тар [Depth		A	В		Mr.		I	 D
mm	in.	SI	Customary	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.
630	24	M20	³ / ₄ – 10	38	1.5	280	11	280 🎤	01	75	3	190	7.5
800	33	M20	$\frac{3}{4} - 10$	38	1.5	300	11.8	300	11.8	75	3	190	7.5
1 000	40	M20	$\frac{3}{4} - 10$	38	1.5	450	17.7	450	17.7	75	3	190	7.5
1 250	50	M20	$\frac{3}{4} - 10$	38	1.5	450	17.7	450	17.7	75	3	190	7.5
1 600	60	M20	$\frac{3}{4} - 10$	38	1.5	600	23.6	600	23.6	75	3	190	7.5

- (b) Dimensions for plain pressure pins and pressure pinholes shall be as specified in Table 20. Pressure pinhole patterns are specified in Table 21.
- (c) Dimensions for headed pressure pins shall be specified in Fig. 7.
- (d) Dimensions of headed pressure pinholes in top surface of bolster shall be as specified in Fig. 8.
- (e) Dimensions of pressure pinholes plugs shall be as specified in Table 22.
 - (f) Pressure Pinhole Location Identification System
- (1) Letters and numbers shall be 13 mm (0.5 in.) high.
- (2) Letters and numbers shall be used in the manner shown in Fig. 9.
- (3) The front of the bolster shall be designated by stamping FRONT in letters that are at least 25 mm (1 in.) high.

5.13 Knockouts

- (a) Provisions for knockouts are optional. Specifications for the requirements shall be provided by the purchaser.
- (b) Knockout bar travel shall be one-third of the length of the slide stroke, but shall not exceed 200 mm (8 in.).
- (c) Total knockout capacity should be 10% of the rated capacity of the press.

5.14 Counterbalance

The counterbalance, when provided, shall meet the following requirements:

- (a) It shall balance the combined weight of the slide, upper die, and attachments.
- (b) The maximum allowable upper die weight is calculated as one-third of the die space in solid steel.
- (c) Pneumatic counterbalance pressure variation shall not exceed 20% during a complete press cycle.

5.15 Machining Specifications

- **5.15.1 Tolerances.** The following tolerances shall apply to die space related dimensions:
- (a) bolster left-to-right and front-to-back dimensions: ±6 mm (±0.25 in.)
 - (b) bolster thickness: ± 0.4 mm (± 0.016 in.)
- (c) bolster mounting slots and holes, from bolster centerlines: ± 0.4 mm (± 0.016 in.)
- (d) die mounting holes, from centerlines of slide: ± 0.4 mm (± 0.016 in.)
- (e) T-slot locations, from centerlines of bolster and slide: ±0.4 mm (±0.016 in.)
- (f) pressure pinholes, from centerlines of bolster and slide: ±0.4 mm (±0.016 in.)
- (g) knockout holes, from front-to-back slide centerline: ± 0.8 mm (± 0.032 in.)
- **5.15.2 Surface Finish.** The following specifications shall apply to surface finishes:
 - (a) bed surface and slide face, R_a : 3.2 μ m (125 μ in.)
 - (b) top and bottom of bolster, R_a : 3.2 μ m (125 μ in.)
- (c) edges of mounting hole pockets, R_a : 6.3 µm $(250 \mu in.)$

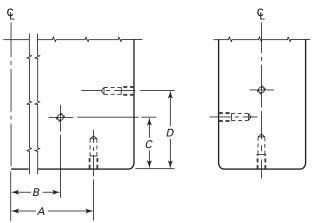


Table 16 Bolster Handling Holes: Two-Point and Four-Point Press

	ed, Right		ap Size Class 3	Тар	Depth	А		В	NE	C		D	
mm	in.	SI	Customary	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.
800	32	M20	³ / ₄ - 10	38	1.5	300	11.8	300	11.8	150	6	230	9
1 250	50	M20	$\frac{3}{4} - 10$	38	1.5	450	17.7	450	17.7	150	6	230	9
1 400	54	M20	$\frac{3}{4} - 10$	38	1.5	450	17.7	450	17.7	150	6	230	9
1 600	60	M20	$\frac{3}{4} - 10$	38	1.5	600	23.6	600	23.6	150	6	230	9
1 800	72	M20	$\frac{3}{4} - 10$	38	1.5	750	29.5	750	29.5	150	6	230	9
2 200	84	M24	1 - 8	50	2	900 🖇	35.4	900	35.4	150	6	230	9
2 500	96	M24	1 - 8	50	2	1 050 🕜	41.3	1 050	41.3	150	6	230	9
2 800	108	M24	1 - 8	50	2	1 200	47.2	1 200	47.2	150	6	230	9
3 100	120	M24	1 - 8	50	2	1350	53.1	1 350	53.1	150	6	230	9
3 400	132	M30	$1^{1}/_{4} - 7$	57	2.25	1 500	59	1 500	59	150	6	230	9
3 700	144	M30	$1^{1}/_{4} - 7$	57	2.25	1 650	65	1 650	65	150	6	230	9
4 000	156	M30	$1^{1}/_{4} - 7$	57	2.25	1 800	70.9	1 800	70.9	150	6	230	9
4 600	180	M38	$1^{1}/_{2} - 6$	70	2.75	2 100	82.7	2 100	82.7	150	6	230	9
5 200	204	M38	$1^{1}/_{2} - 6$	70.	2.75	2 400	94.5	2 400	94.5	150	6	230	9

- **5.15.3 Chamfers.** The following components shall be provided with the specified chamfers:
- (a) all bolster edges and shank holes: 6 mm (0.25 in.) × 45 deg
 - (b) pressure pinholes: 1.5 mm (0.06 in.) \times 45 deg
- (c) knockout pin ends and knockout holes: 1.5 mm (0.06 in.) × 45 deg

6 ACCEPTANCE CONDITIONS

6.1 Press Accuracy

The press shall be precision leveled in order to prevent cross-corner binding of the slide in the gibs and to ensure a level datum plane on which to base measurements of press accuracy. The validity of the test is dependent on this datum plane being flat and level within accepted limits. The bed shall be established as the datum plane for leveling the press. The bolster (or bed) surface shall be established as the datum plane for slide parallelism and alignment. See Fig. 10.

6.1.1 Acceptance Limits for Level. The datum plane shall be level within 0.04 mm/m (0.0005 in./ft) of die

space dimensions, as measured at the centers of the left-to-right and front-to-back dimensions. Measurements shall be made with a 10 second level having a sensitivity of 0.04 mm per graduation per meter (0.0005 in./ft).

6.1.2 Flatness: Bed and Slide Face. Flatness of the tool attachment surface shall be within 0.04 mm/m (0.0005 in./ft) with a maximum total not to exceed 0.25 mm (0.01 in.).

NOTE: The acceptance condition of flatness of bed and slide shall be made at the time of machining by the supplier.

6.1.3 Bolster Flatness and Parallelism. See Fig. 11.

- **6.1.4** Parallelism Between Slide Face and Bed or Bolster Surface. Parallelism between the slide face and the bed or bolster surface, measured front-to-back and left-to-right, shall be within the following maximum tolerance (see Fig. 12.):
- (a) at the end of the slide stroke: 0.08 mm/m (0.001 in./ft)
- (b) at mid-stroke (both closing and opening): 0.25 mm/m (0.003 in./ft)

Measurements shall be made:

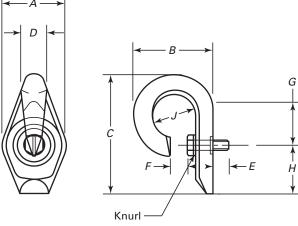


Table 17 Bolster Handling Hook Dimensions

	Rated Capacity										
	27 kN (3 tons)		53 kN (6 tons)		80 kN (9 tons)		134 kN (15 tons)				
Dimension	mm	in.	mm	in.	mm	ķ in.	mm	in.			
A	76	3	89	3.5	102	4	114	4.5			
В	130	5.13	166	6.63	203	8	241	9.5			
С	189	7.44	229	9	268	10.57	308	12.13			
D	29	1.13	38	1.5	51	2	64	2.5			
Ε	35	1.38	44	1.75	52	2.06	64	2.5			
F	35	1.38	41	1.63	6 51	2	51	2			
G	70	2.75	89	3.5	108	4.25	121	4.75			
Н	73	2.88	89	3.5	102	4	114	4.5			
J	76	3	89	3.50	102	4	114	4.5			

Table 18 Bolster Handling Hook Bolt Dimensions

Сар	acity	Dia	neter	T	Thread		
kN	tons	mm	in.	SI 🌙	Customary		
27	3	20	0.75	M20	10NC - 3		
53	6	24	1.0	M24	8NC - 3		
80	9	30	1.25	₩ 30	7NC - 3		
134	15	38	1.5	M38	6NC – 3		

- (a) with the adjustment up
- (b) under no load and set for normal running conditions (manufacturers will advise)
- (c) with sufficient counterbalance force to overcome the cumulative clearances (lost motion) of the press drive

EXAMPLE: The parallelism of a press with a $2\,500$ mm (100 in.) dimension should be within 0.2 mm (0.008 in.) at the end of the slide stroke and 0.6 mm (0.024 in.) at mid-stroke.

6.1.5 Squareness: Slide Travel. The total runout F.I.M. (full indicator movement) of slide travel shall not exceed 0.1 mm (0.004 in.) for the first 100 mm (4 in.) of travel, and shall not exceed 0.01 mm (0.0004 in.) for each additional 100 mm (4 in.) of travel. See Fig. 13.

Measurements shall be made:

(a) both left-to-right and front-to-back

- (b) for the one-third of the slide travel that precedes the end of the stroke
- (c) with sufficient counterbalance force to overcome the cumulative clearances (lost motion) of the press drive
- **6.1.6 Parallelism: Die Cushion Pin Plate.** Parallelism between the surface of the die cushion pin plate and the top of the bed shall be parallel within 0.33 mm/m (0.004 in./ft) of die cushion dimensions, both left-to-right and front-to-back, not to exceed 0.75 mm (0.030 in.).

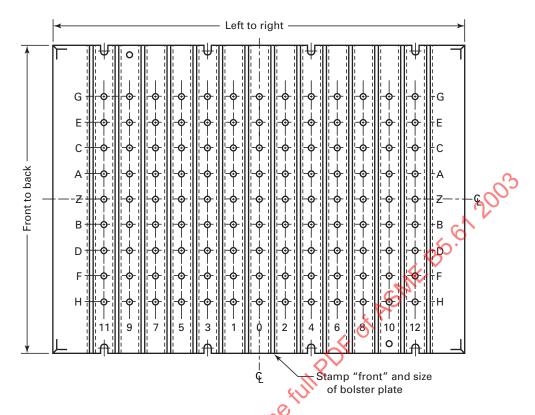
6.2 Bed and Slide Deflection

The allowable deflection of the bed and slide shall comply with the design criteria specified in para. 4.4(b).

6.3 Slide Parallelism Under Load

The following is the procedure for checking parallelism of a mechanical press slide under load (see Fig. 14):

- (a) Utilize a matched set of load cells, stanchions and spacers.
 - (b) Verify that the press slide is at bottom dead center.
- (c) Adjust the slide down to make contact with the load cells.
- (*d*) From top dead center, cycle press at full speed and take readings from load cell amplifier.
- (e) Adjust the slide down in small increments to increase load to 50% to 70% of rated capacity.



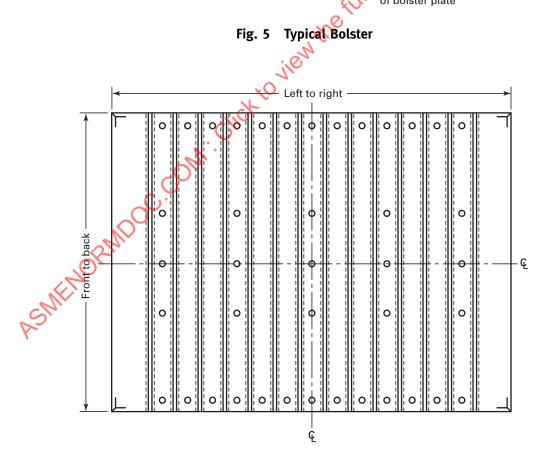


Fig. 6 Typical Slide

Table 19 Number of T-Slots

	Bed, Left to Right		
mm	in.	of T-Slots	
630	24	4	
800	32	4	
1 000	40	6	
1 250	50	8	
1 400	54	8	
1 600	60	10	
1 800	72	10	
2 200	84	12	
2 500	96	14	
2 800	108	16	
3 100	120	18	
3 400	132	20	
3 700	144	22	
4 000	156	24	
4 600	180	28	
5 200	204	32	

(f) Record all readings. (Calibrate the load monitor if the press is so equipped.)

An acceptable variance (using load cells) within all corners is 1.5% of the rated press capacity.

EXAMPLE: For $10\,000~kN$ (1,100 ton), a variance of 150~kN (16.5 tons) is acceptable.

7 HEALTH AND SAFETY

7.1 Ergonomics

Ergonomic considerations in the design of power presses are provided in ANSI B11-TR1, Ergonomic Guidelines for the Design, Installation and Use of Machine Tools.

7.2 Safeguarding

Safeguarding requirements in the use of power presses are provided in the following:

- (a) Code of Federal Regulations (CFR) (mandated by OSHA)
 - (1) 29 CFR 1910.147
 - (2) 29 CFR 1910.212
 - (3) 29 CFR 1910.217
 - (4) 29 CFR 1910.219
 - (b) American National Standards Institute (ANSI)
 - (1) ANSI B11.1
 - (2) ANSI B11.2
 - (3) ANSI B11.19
 - (4) ASME B15.1
 - (5) ANSI/NFPA 79
 - (c) National Safety Council (General Requirements)
- (1) Accident Prevention Manual for Business and Industry (Volumes 1 and 2)
 - (2) Power Press Safety Manual

8 INFORMATION AND INSTRUCTIONS

8.1 Identification

The manufacturer shall provide data plates of durable material, permanently attached, to display information applicable to the press and its accessories. Letters and numbers shall be at least 3 mm (0.12 in.) high.

- **8.1.1 Press Data Plate.** A data plate shall be attached to the front right hand side of the press, its height not to exceed 2 000 mm (80 in.) from floor level. See Figs. 15 and 16 for examples.
- **8.1.2 Counterbalance Data Plate.** A data plate shall be attached adjacent to the counterbalance system pressure control. See Fig. 17 for an example.

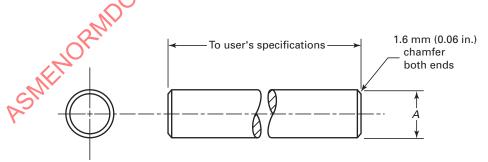
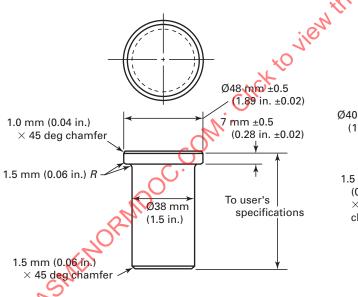


Table 20 Plain Pressure Pin

Press Ca	pacity		4	Pressure Pinhole Diameter		
kN	tons	mm	in.	mm	in.	
250-2 000 2 000-25 000	30-225 225-2,810	25 38	1.0 1.5	27 40	1.06 1.6	

		Front to Back		Left to Right			
Rows of		Capaci	ension	Bed Din	Rows of	ension	Bed Dime
Holes	tons	kN	in.	mm	Holes	in.	mm
3			23.6	600	3	24	630
3 5			31.5	800	3	32	800
5			35.4	900	5	40	1 000
			39.4	1 000	7	50	1 250
5 5 7			44.1	1 120	7	54	1 400
7	< 450	< 4 000	49.2	1 250	9	60	1 600
5	≥ 450	≥ 4 000					
	00				9	72	1 800
7			55.1	1 400	11	84	2 200
	< 450	< 4 000	63	1 600	13	96	2 500
9 7	ó 450	≥ 4 000					
	5				15	108	2 800
11	< 450	< 4 000	70.8	1 800	17	120	3 100
9	≥ 450	≥ 4 000					
		S			19	132	3 400
11			78.7	2 000	21	144	3 700
11		× ,	86.6	2 200	23	156	4 000
13		7, 0	94.5	2 400	27	180	4 600
15	< 1,125	< 10 000	102.4	2 600	31	204	5 200
13	≥ 1,125	≥ 10 000					
15	•••		110.2	2 800			
17	•••		118.4	3 000			

Table 21 Pressure Pinhole Patterns



Ø50 mm ±0.7 (1.97 in. ± 0.03) 10 mm ±0.05 (0.39 in. ± 0.02) 1.5 mm (0.06 in.) × 45 deg chamfer (0.04 in.) R

Fig. 8 Headed Pressure Pinhole

8.1.3 Die Cushion Data Plate. When a die cushion is provided, a data plate shall be attached adjacent to the die cushion system pressure control. See Fig. 18 for an example.

Fig. 7 Headed Pressure Pin

- **8.1.4 Clutch/Brake Data Plate.** When a pneumatic clutch/brake is provided, a data plate shall be attached adjacent to the pressure regulator to indicate clutch/brake air pressure for rated capacity.
- **8.1.5** Lubrication and Operating Fluid Data Plate. Lubrication and operating fluid data plates, when provided, shall be attached near lubricant fill points.
- **8.1.6 Press Designation.** The designation of presses shall be displayed on the front of the press crown and shall be in accordance with the system depicted on Fig. 19.

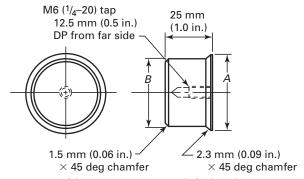


Table 22 Pressure Pinhole Plug

	A		В
mm	in.	mm	in.
29.6	1.14	25	0.98
29.6 42.6	1.68	38	1.50

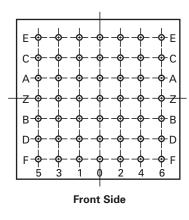


Fig. 9 Pressure Pinhole Location Identification
System

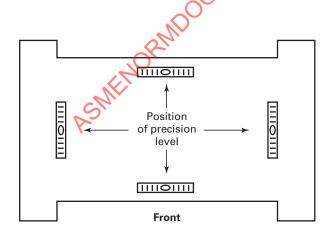


Fig. 10 Establishing the Bed as the Datum Plane

EXAMPLE: $SE2 - 4\,000 - 2\,500 \times 1\,400$ designates a single straight side press with a two-point eccentric gear drive, $4\,000$ kN capacity, and $2\,500$ mm $\times 1\,400$ mm die space.

8.1.7 Serial Number

- (a) The press serial number shall be permanently marked on the left front upright below the gibs, in letters and numbers at least 6 mm (0.25 in.) high.
- (b) The press serial number shall also be permanently marked in a readily visible location on the press slide.
- (c) For presses with a four-piece tie-rod frame, the press serial number shall also be permanently marked in readily visible locations on the right hand upright, crown, and bed.

8.2 Shipping and Assembly Provisions

- (a) Junction boxes and unions shall be located to facilitate press assembly without removing wiring, conduit, piping, or lubrication lines.
- (b) Each subassembly (uprights, crown, slide, and bed) shall be clearly and permanently identified with the following information:
 - (1) press serial number
 - (2) weight of each major subassembly
- (3) the word FRONT to designate the front of the press
- Ottlity connections shall be located so that the connections can be readily made after the press is erected.
- (d) Properly designed handling holes or hooks shall be provided for safe handling of each major subassembly. Handling holes or hooks shall be located to avoid interference with accessories and mounted on a machined surface.
- (e) Safety cables or straps shall be provided to secure major components that are mounted external to the press frame (i.e., motors, surge tanks, etc.).

8.3 Instruction Manual

- (a) The manufacturer shall provide a minimum of two instruction manuals on proper:
 - (1) installation
 - (2) operation
 - (3) maintenance
 - (4) safeguarding
- (b) For mechanical power presses, the instruction manual shall include the following information:
 - (1) rated capacity based on drive torque
- (2) press capability based on usable flywheel energy
 - (3) slide velocity characteristics

This information can be combined into a single press capability graph such as the example shown in Figs. 20 and 21.

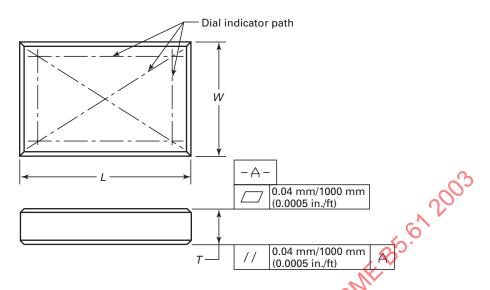


Fig. 11 Bolster Flatness and Parallelism

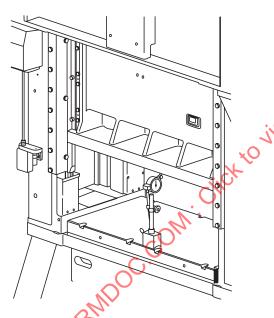


Fig. 12 Checking Parallelism From Slide Face to Bed or Bolster Surface

9 DECLARATION OF MANUFACTURER'S COMPLIANCE

Upon request, the machine manufacturer shall provide a certificate of compliance with this Standard. The certificate, entitled "ASME B5.61 COMPLIANCE," shall include the following information:

- (a) manufacturer
- (b) press designation
- (c) machine model
- (d) machine serial number
- (e) date

10 REFERENCE STANDARDS

10.1 Normative References

ANSI B11.TR-1-1995, Ergonomic Guidelines for the Design, Installation and Use of Machine Tools

ANSI B11.1-2002, Machine Tools — Mechanical Power Presses — Safety Requirements for Construction, Care, and Use

ANSI B11.2-1995 (R2002), Hydraulic Power Presses ANSI B11.19-1990 (R1996), Performance Criteria for Safeguarding Machine Tools

Publisher: American National Standards Institute (ANSI), 25 West 43rd Street, New York, NY 10036

ASME B5.1M-1985 (R1998), T-Slots — Their Bolts, Nuts, and Tongues

ASME B5.49-1998, Glossary of Power Press Terms

ASME B5.51M-1979 (R2002), Preferred SI Units for Machine Tools

ASME B15.1-2000, Safety Standard for Mechanical Power Transmission Apparatus

Publisher: The American Society of Mechanical Engineers (ASME International), Three Park Avenue, New York, NY 10016-5990; Order Department: 22 Law Drive, Box 2300, Fairfield, NJ 07007-2300

29 CFR 1910.147, The Control of Hazardous Energy (Lockout/Tagout)

29 CFR 1910.212, General Requirements for All Machines 29 CFR 1910.217, Mechanical Power Presses

29 CFR 1910.219, Mechanical Power-Transmission Apparatus

Publisher: Superintendent of Documents, U.S. Government Printing Office, Washington, DC 20402-9325

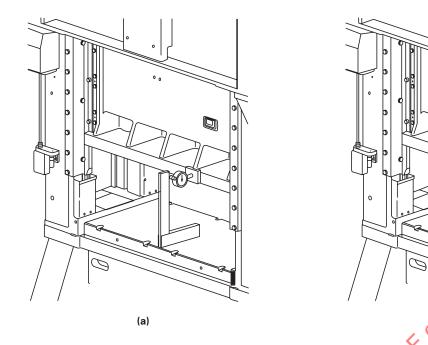


Fig. 13 Checking Squareness of Slide Travel

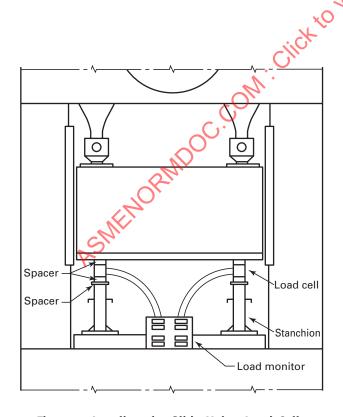


Fig. 14 Leveling the Slide Using Load Cells

NFPA 79-1997, Electrical Standard for Industrial Machinery

Publisher: National Fire Protection Association (NFPA), 1 Batterymarch Park, Quincy, MA 02269-9101

Accident Prevention Manual for Business and Industry (Volumes 1 and 2)

Power Press Safety Manual

Publisher: National Safety Council (NSC), 1121 Spring Lake Drive, Itasca, IL 60143-3201

10.2 Informative References

ANSI B93.114M-1987, Pneumatic Fluid Power — Systems Standard for Industrial Machinery

Publisher: American National Standards Institute (ANSI), 25 West 43rd Street, New York, NY 10036

ASME B5.52-2003, Mechanical Power Presses: General Purpose, Single Point, Gap Type

Publisher: The American Society of Mechanical Engineers (ASME International), Three Park Avenue, New York, NY 10016-5990; Order Department: 22 Law Drive, Box 2300, Fairfield, NJ 07007-2300

ISO 9188:1993, Machine Tools — Straight-sided singleaction mechanical power presses from 400 kN up to and including 4 000 kN nominal force — Characteristics and dimensions

PRESS DATA	
SERIAL NUMBER	
MODEL NUMBER	
CAPACITY kN (tons) at] mm (in.)
USABLE FW ENERGY kN•m (intons) at	SPM
STROKES PER MINUTE]SPM
SHUTHEIGHT-SLIDE TO BED, SDAU]mm (in.)
ADJUSTMENT OF SLIDE	mm (in.)

Fig. 15 Press Data Plate: Mechanical Press

PRESS DATA	4/
SERIAL NUMBER	3/11/
MODEL NUMBER	
CAPACITY kN (tons)	
SPEED AT FULL CAPACITY	mm/s (IPM)
SHUTHEIGHT-SLIDE TO BED, SDAU	mm (in.)
ADJUSTMENT OF SLIDE	mm (in.)

Fig. 16 Press Data Plate: Hydraulic Press

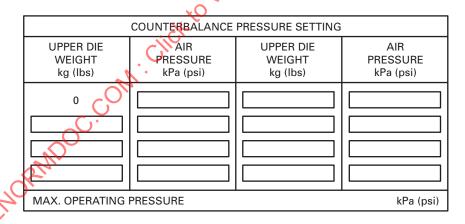


Fig. 17 Counterbalance Data Plate

ISO 9189:1993, Machine Tools — Straight-sided highspeed mechanical power presses from 250 kN up to and including 4 000 kN nominal force — Characteristics and dimensions

Publisher: International Organization for Standardization (ISO), 1 rue de Varembé, Case Postale 56, CH-1211, Genève 20, Switzerland/Suisse

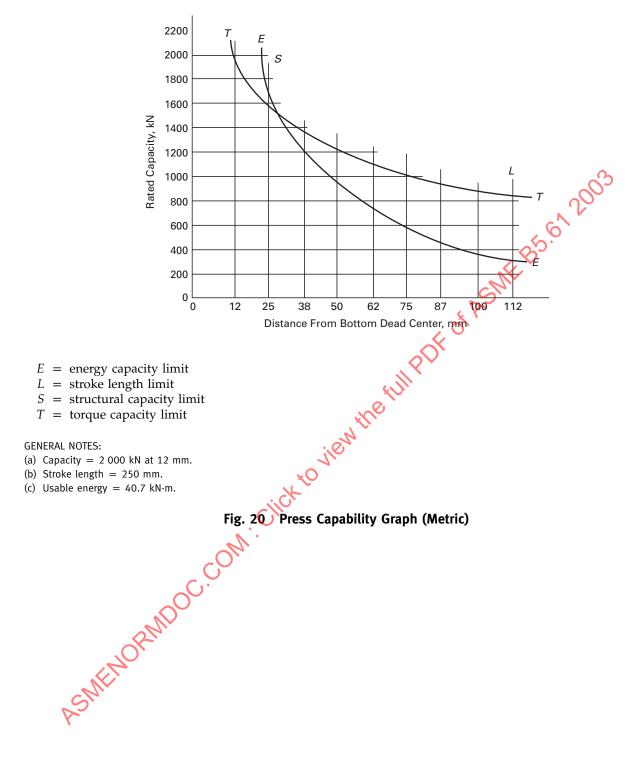
NFPA/T2.24.1 R1-2000, Hydraulic Fluid Power — Systems Standard for Stationary Industrial Machinery — Supplement to ISO 4413:1998, Hydraulic Fluid Power — General Rules Relating to Systems

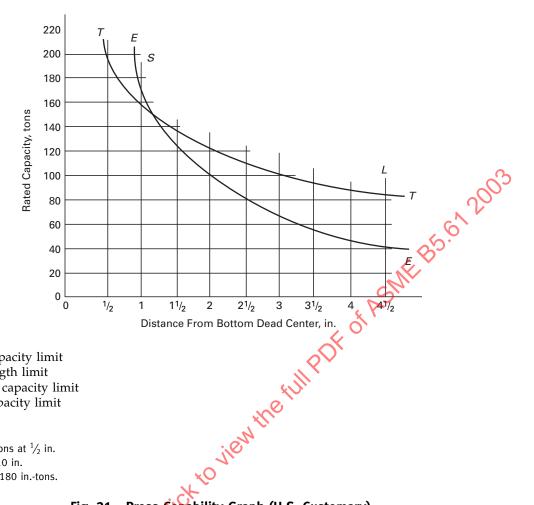
Publisher: National Fluid Power Association (NFPA), 3333 North Mayfair Road, Milwaukee, WI 53222-3219

6 = special manufacturer's designation

DIE CUSHION DATA	
SERIAL NUMBER	
MODEL	
STROKEmm (in.)	
CAPACITY kN (tons) at kPa (psi)	
MAX. OPERATING PRESSURE kPa (psi)	ص م
Fig. 18 Die Cushion Data Plate	6/3003
Fig. 18 Die Cushion Data Plate Marking system for identifying press 1 2 3 4 5 -	ses:
 S = single action straight side press 1 = type of press: C = crankshaft or eccentric shaft E = eccentric gear 	
H = hydraulic $L = link drive$	
2 = number of slide connections	
3 = rated capacity,kN	
4 = left to-right dimension of bed and bolster, mm	
5 = front-to-back dimension of bed and bolster, mm	

Fig. 19 Press Designation System





E = energy capacity limitL = stroke length limitS =structural capacity limit T = torque capacity limit

GENERAL NOTES:

- (a) Capacity = 225 tons at $\frac{1}{2}$ in.
- (b) Stroke length = 10 in.
- (c) Usable energy = 180 in.-tons.

Fig. 21 Press Capability Graph (U.S. Customary)

MANDATORY APPENDIX I MECHANICAL POWER PRESS CAPACITY ABOVE RATING POINT OF 12.7 mm (0.5 in.)

Table	l-1	Percent	of	Rated	Capacity	v
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					Dista	ance Fr	m	ttom De im n.)	ead Cent	er,		6	\ \?\
Stro	ke	12.7	19	25	38	50	75	100	125	150	200	250	300
mm	in.	(0.5)	(0.75)	(1)	(1.5)	(2)	(3)	(4)	(5)	(6)	(8)	(10)	(12)
80	3	100	87	80							'M'		
100	4	100	86	78	71								
125	5	100	85	76	68	65				81			
150	6	100	84	75	66	61				O.			
200	8	100	83	74	63	58	53						
250	10	100	83	73	62	56	50	47 🕢	\circ				
300	12	100	83	73	61	55	48	44	43				
400	16	100	83	72	60	53	46	42	39	38			
500	20	100	82	72	60	53	45	40	37	36	34		
600	24	100	82	72	59	52	44	9 39	36	34	32	31	
800	32	100	82	71	59	52	43	38	35	33	30	28	27

The "slider crank" motion, imparted by a crankshaft, eccentric shaft, or eccentric gear, produces the reciprocating motion of the press slide. The changing mechanical advantage that results from the changing geometry of the crank arm position, relative to the slide connection(s), converts the constant torque of the rotating drive members into a varying linear force when applied by the slide. This force is at its minimum when the crank arm and connection form a right angle (near midstroke).

It is at its maximum when the slide approaches the end of its travel.

EXAMPLES:

- (1) Capacity of 4 000 kN press, 400 mm stroke, 50 mm from bottom of stroke. From Table I-1, the capacity is 53% of rated capacity at 50 mm from bottom dead center (BDC). Capacity: 4 000 kN \times 0.53 = 2120 kN
- (2) Capacity of 450 ton, 8 in. stroke, 2 in. from bottom of stroke. From Table I-1, the capacity is 58% of rated capacity at 2 in. from BDC. Capacity: 450 tons \times 0.58 = 238.5 tons